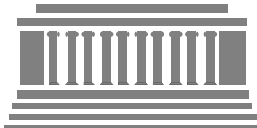


# Remarks on the Birefringence in Stress- Controlled Linear Viscoelasticity:

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Lecture Notes available at the web site:

[www.chem.cmu.edu/Berry/birefringence.pdf](http://www.chem.cmu.edu/Berry/birefringence.pdf)

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## Linear Viscoelasticity:

$$R(t) = J(t) - t/\eta = J_\infty - [J_\infty - J_0]\alpha(t)$$
$$G(t) = G_e + [G_0 - G_e]\varphi(t)$$

Here,

$\eta$  is the (linear) viscosity, with  $1/\eta = 0$  for a fluid,

$G_e$  is the equilibrium modulus, with  $G_e = 0$  for a solid,

$G_0$  is the "instantaneous" modulus, with  $J_0 G_0 = 1$ , and

$J_\infty$  is the limit of  $R(t)$  for large  $t$ , with values discussed below

$$1 = \frac{1}{t} \int_0^t du G(t-u) J(u)$$

$$B(t) = B_e - [B_e - B_0]\beta(t)$$

$$K(t) = K_e + [K_0 - K_e]\kappa(t)$$

Incompressible linear elastic solid:  $K \gg G \approx E/3$  or, equivalently,  $B \ll J \approx 3D$ .

$$\epsilon_{ij} = \frac{1}{2} \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right); \mathbf{u} \text{ is the displacement vector}$$

$$2\epsilon_{ij}(t) = \int_{-\infty}^t ds \left\{ J(t-s) \left[ \frac{\partial S_{ij}(s)}{\partial s} - \frac{1}{3} \delta_{ij} \frac{\partial S_{\alpha\alpha}(s)}{\partial s} \right] + (2/9) \delta_{ij} B(t-s) \frac{\partial S_{\alpha\alpha}(s)}{\partial s} \right\}$$

$$S_{ij}(t) = \int_{-\infty}^t ds \left\{ 2G(t-s) \left[ \frac{\partial \epsilon_{ij}(s)}{\partial s} - \frac{1}{3} \delta_{ij} \frac{\partial \epsilon_{\alpha\alpha}(s)}{\partial s} \right] + \delta_{ij} K(t-s) \frac{\partial \epsilon_{\alpha\alpha}(s)}{\partial s} \right\}$$

Coleman, B. D.; Dill, E. H.; Toupin, R. A. "A phenomenological theory of streaming birefringence" *Arch. Rational Mech. Anal.* **1970**, 39, 358-99.

$$n_{ij}(t) = \int_{-\infty}^t ds \left\{ J_n(t-s) \left[ \frac{\partial S_{ij}(s)}{\partial s} - \frac{1}{3} \delta_{ij} \frac{\partial S_{\alpha\alpha}(s)}{\partial s} \right] + \delta_{ij} [n_o + (2/9) B_n(t-s) \frac{\partial S_{\alpha\alpha}(s)}{\partial s}] \right\}$$

$$n_{ij}(t) = \int_{-\infty}^t ds \left\{ 2G_n(t-s) \left[ \frac{\partial \epsilon_{ij}(s)}{\partial s} - \frac{1}{3} \delta_{ij} \frac{\partial \epsilon_{\alpha\alpha}(s)}{\partial s} \right] + \delta_{ij} [n_o + K_n(t-s) \frac{\partial \epsilon_{\alpha\alpha}(s)}{\partial s}] \right\}$$

$$1 = G(0)J(t) + \int_0^t du J(t-u) \frac{\partial G(u)}{\partial u}$$

$$J_n(t) = G_n(0)J(t) + \int_0^t du J(t-u) \frac{\partial G_n(u)}{\partial u}$$

**NOTE:**  $J_n(t)$  is a constant if  $G_n(t)/G(t)$  is independent of  $t$ .

## Deviatoric Components:

Strain-defined history:

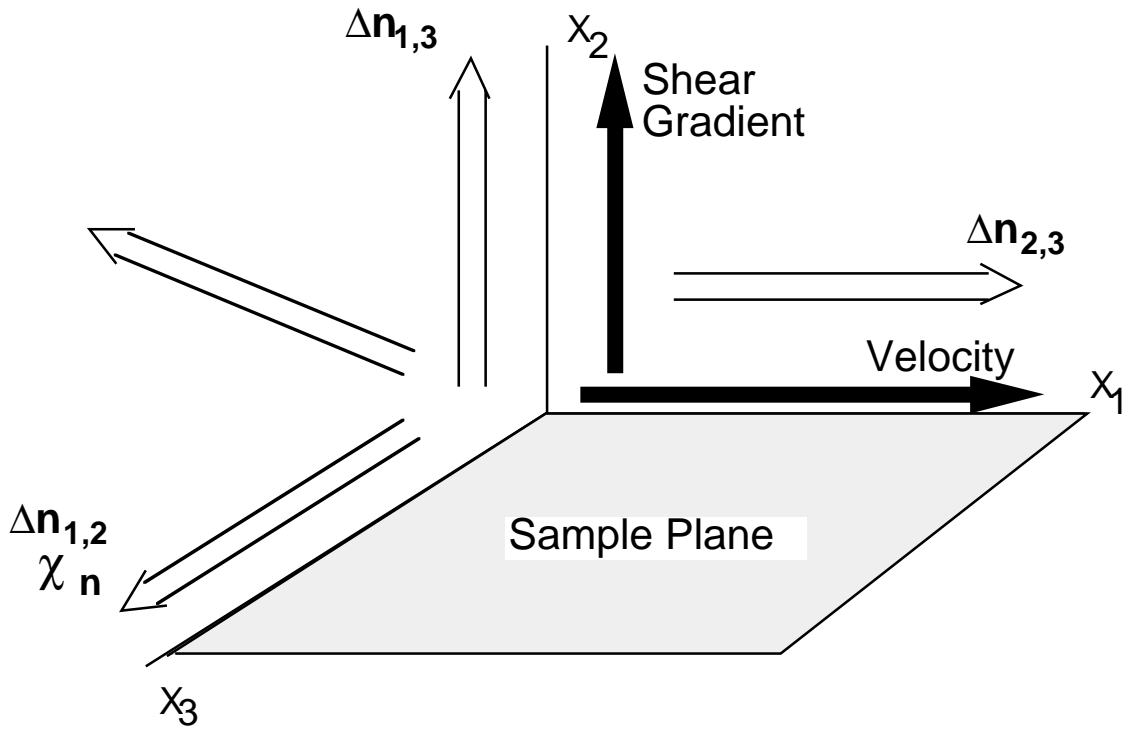
$$n_{12}(t) = G_n(0)\epsilon_{12}(t) + \int_0^\infty du \epsilon_{12}(t-u) \frac{\partial G_n(u)}{\partial u}$$

$$n_{11}(t) - n_{22}(t) = G_n(0)[\epsilon_{11}(t) - \epsilon_{22}(t)] + \int_0^\infty du [\epsilon_{11}(t-u) - \epsilon_{22}(t-u)] \frac{\partial G_n(u)}{\partial u}$$

Stress-defined history:

$$n_{12}(t) = J_n(0)S_{12}(t) + \int_0^\infty du S_{12}(t-u) \frac{\partial J_n(u)}{\partial u}$$

$$n_{11}(t) - n_{22}(t) = J_n(0)[S_{11}(t) - S_{22}(t)] + \int_0^\infty du [S_{11}(t-u) - S_{22}(t-u)] \frac{\partial J_n(u)}{\partial u}$$



$$\Delta n_{1,2}(t) = [n_{11}(t) - n_{22}(t)]\cos[2\chi_n(t)] + 2n_{12}(t)\sin[2\chi_n(t)]$$

$$\cot[2\chi_n(t)] = [n_{11}(t) - n_{22}(t)]/2n_{12}(t)$$

Shear deformation along  $x_1$

$$\Delta n_{1,2}(t)\sin[2\chi_n(t)] = 2n_{12}(t); \quad \pi/4 > \chi_n(t) > 0$$

Uniaxial elongation along  $x_1$

$$\Delta n_{1,2}(t) = n_{11}(t) - n_{22}(t); \quad \chi_n(t) = 0.$$

## Linear elastic solid:

$$(\chi_n \approx \pi/4)$$

$$\partial G_n(t)/\partial t = \partial J_n(t)/\partial t = 0$$

### Strain-defined:

$$n_{12}(t) = G_n(0)\epsilon_{12}(t)$$

### Stress-defined:

$$n_{12}(t) = J_n(0)S_{12}(t) = G_n(0)J(t)S_{12}(t) = G_n(0)\epsilon_{12}(t)$$

**Linear viscoelastic fluid in steady state deformations:**  
**Steady-state shear flow in the linear response ( $\chi_n \approx \pi/4$ ):**

Strain-defined:

$$\gamma(t) = \dot{\gamma}t$$

$$\Delta n_{ss} = 2n_{12}(t) = 2 \lim_{t \rightarrow \infty} \int_0^t du G_n(t-u) \frac{\partial \gamma(s)}{\partial s} = 2\dot{\gamma} \int_0^\infty du G_n(u)$$

Assume  $G_n(t) = C \times G(t)$ :

$$\Delta n_{ss}/2C = \dot{\gamma} \int_0^\infty du G(u) = \eta \dot{\gamma} = (1/J_s) \hat{\gamma}_R(\dot{\gamma})$$

with  $\hat{\gamma}_R(\dot{\gamma})$  the total strain recoil on cessation of steady-state flow at shear rate  $\dot{\gamma}$ .

Stress-defined:

$$\sigma(t) = \sigma_o = \eta \dot{\gamma}_{ss} \text{ for } t \geq 0$$

$$\Delta n_{ss} = 2n_{12}(t) = 2 \lim_{t \rightarrow \infty} \int_0^t du J_n(t-u) \frac{\partial \sigma(s)}{\partial s} = 2J_n(\infty) \eta \dot{\gamma}_{ss}$$

$$\lim_{t \rightarrow \infty} \hat{\gamma}_R(t) = \lim_{t \rightarrow \infty} \sigma_o \int_0^t du R(t-u) = \sigma_o J_s = \eta \dot{\gamma}_{ss} J_s$$

But from above,

$$\Delta n_{ss}/2C = \eta \dot{\gamma}_{ss} = (1/J_s) \hat{\gamma}_R(\dot{\gamma}_{ss})$$

Consequently, for correspondence,  $J_n(\infty) = C$

## Steady-state oscillatory deformation in the linear response:

$$(\chi_n \approx \pi/4)$$

Strain-defined:

$$\begin{aligned}\sigma(t) &= \gamma_o \{ G'(\omega) \sin(\omega t) + G''(\omega) \cos(\omega t) \} \\ G'(\omega) &= G_e + \omega [G_o - G_e] \int_0^\infty ds \varphi(s) \sin(\omega s) \\ G''(\omega) &= \omega [G_o - G_e] \int_0^\infty ds \varphi(s) \cos(\omega s)\end{aligned}$$

$$n_{12}(t) = \gamma_o \{ G'_n(\omega) \sin(\omega t) + G''_n(\omega) \cos(\omega t) \}$$

If  $G_n(t) = C G(t)$ , then

$$G'_n(\omega) = C G'(\omega) \quad \text{and} \quad G''_n(\omega) = C G''(\omega)$$

e.g., for small  $\omega$ :  $G'_n(\omega) \propto G'(\omega) \propto \omega^2$  and  $G''_n(\omega) \propto G''(\omega) \propto \omega$ . [100]

Stress-defined:

$$\begin{aligned}\gamma(t) &= \sigma_o \{ J'(\omega) \sin(\omega t) - J''(\omega) \cos(\omega t) \} \\ J'(\omega) &= J_\infty - \omega [J_\infty - J_o] \int_0^\infty ds \alpha(s) \sin(\omega s) \\ J''(\omega) &= (1/\omega \eta) + \omega [J_\infty - J_o] \int_0^\infty ds \alpha(s) \cos(\omega s) \\ n_{12}(t) &= \sigma_o \{ J'_n(\omega) \sin(\omega t) - J''_n(\omega) \cos(\omega t) \}\end{aligned}$$

Since  $J'_n(\omega) = G'_n(\omega) J'(\omega)$ :

$$\begin{aligned}J'_n(\omega) &= G'_n(\omega) J'(\omega) + G''_n(\omega) J''(\omega) \\ J''_n(\omega) &= G''_n(\omega) J'(\omega) - G'_n(\omega) J''(\omega)\end{aligned}$$

If  $G_n(t) = G(t)$ :

$$\begin{aligned}J'_n(\omega)/C &= G'(\omega) J'(\omega) + G''(\omega) J''(\omega) \\ J''_n(\omega)/C &= G''(\omega) J'(\omega) - G'(\omega) J''(\omega)\end{aligned}$$

For small  $\omega$ :

$$\begin{aligned}J'_n(\omega)/C &= (\eta J_s \omega)^2 + 1 \approx 1 \\ J''_n(\omega)/C &= (\eta J_s \omega) - (\eta J_s \omega) = 0\end{aligned}$$

For small  $\omega$ , the birefringence is predicted to be exactly in phase with the oscillating stress, as expected: Note that  $J''_n(\omega)$  provides no input on  $\eta$ .

Application of  $G_n(t) = C G(t)$  for all  $t$  would require this same behavior for all  $\omega$ .

Transient shear flow in the linear response ( $\chi_n \approx \pi/4$ ):  
Strain-defined:

Approximation  $G_n(t)/G(t) = C$ :

$$n_{ij}(t) = 2C \int_0^t ds G(t-s) \left[ \frac{\partial \varepsilon_{ij}(s)}{\partial s} - \frac{1}{3} \delta_{ij} \frac{\partial \varepsilon_{\alpha\alpha}(s)}{\partial s} \right]$$

For a shear deformation:

$$\Delta n(t) = 2C\sigma(t) = 2C \int_0^t du G(t-u) \frac{\partial \gamma(u)}{\partial u}$$

Stress relaxation following a small step-strain  $\gamma_0$ :

$$\Delta n(t) = 2C\gamma_0 G(t)$$

Stress-growth in low shear flow at shear rate  $\dot{\gamma}$ :

$$\Delta n(t) = 2C\dot{\gamma} \int_0^t du G(u)$$

Stress-defined:

$$n_{ij}(t) = (C/J_\infty) \int_0^t ds J_n(t-s) \left[ \frac{\partial S_{ij}(s)}{\partial s} - \frac{1}{3} \delta_{ij} \frac{\partial S_{\alpha\alpha}(s)}{\partial s} \right]$$

If  $J_n(t) = C$ , consistent with  $G_n(t) = G(t)$ , then  $\Delta n$  in creep would step up at creep onset, and the remain constant--**this does not seem reasonable**.

Suppose  $J_n(t) = C R(t)/J_s$

$$\Delta n(t) = 2(C/J_\infty) \int_0^t du R(t-u) \frac{\partial \sigma(u)}{\partial u}$$

The total recoverable strain  $\hat{\gamma}_R(t)$  obtained a long time after the stress is reduced to zero at time  $t$  following an arbitrary stress history up to  $t$  is given by

$$\hat{\gamma}_R(t) = \int_0^t du R(t-u) \frac{\partial \sigma(u)}{\partial u}$$

Consequently,

$$\Delta n(t) = 2(C/J_\infty) \hat{\gamma}_R(t)$$

**i.e., the birefringence provides a measure of the recoverable deformation in the chains.**

For recovery starting at time  $T_e$  during stress relaxation:

$$\hat{\gamma}_R(T_e) = \gamma_0 \{ 1 - \eta^{-1} \int_0^{T_e} du G(u) \}$$

Not equal to  $\gamma_0 G(t)$  unless  $G(t) \propto \exp(-t/\tau)$ , in which case  $R(t) = J_s$

## Second-Order Nonlinear Behavior:

$$S_{\alpha\beta}(t) = - \int_0^\infty du Q_{\alpha\beta}^o(t,u) \frac{\partial G(t-u)}{\partial u} - \delta_{\alpha\beta} P$$

Shear deformation along  $x_1$  and shear gradient along  $x_2$ :

$$\mathbf{Q}_{sh}^o = \begin{pmatrix} 1 + \gamma(t,u)^2 & \gamma(t,u) & 0 \\ \gamma(t,u) & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}; \quad \gamma(t,u) = \int_u^t ds \dot{\gamma}(s)$$

Uniaxial elongational deformation with deformation along  $x_1$ :

$$\mathbf{Q}_{el}^o = \begin{pmatrix} \lambda(t,u)^2 & 0 & 0 \\ 0 & \lambda(t,u)^{-1} & 0 \\ 0 & 0 & \lambda(t,u)^{-1} \end{pmatrix}; \quad \ln[\lambda(t,u)] = \int_u^t ds \dot{\lambda}(s)$$

for the strain- and stress-defined experiments, respectively, where  $G_n'(\omega)$  is defined in terms of  $G_n(t)$  in a way analogous to the relation between  $G'(\omega)$  and  $G(t)$ , etc. If it is assumed that  $G_n(t)/G(t) = C$  for all  $t$ , then for the stress-defined history. Dynamic birefringence measurements in the 1,2-plane with small  $\gamma_0$  appear to be in accord with the stress-optic approximation over limited ranges in  $\omega$  near the "terminal response" for which Dynamic measurements of  $\Delta n_{1,3}(t)$  in the 1,3-plane with small  $\gamma_0$ , for which  $\Delta n_{1,3}(t) = C(1 - \hat{\psi})N_1(t)$  with  $N_1(t)$  given by the expression for nonlinear normal stress in oscillatory shear deformation discussed above using the strain tensor  $\mathbf{Q}^o$ , have been used to estimate  $\hat{\beta}$  on the basis that  $\hat{\psi} = \hat{\beta}$ , as expected with the stress-optic approximation.[100] Nevertheless, the stress-optic approximation is known to be inadequate in some

Step strain of  $\gamma_0$ :

$$N_1(t, \gamma_0) \approx \gamma \sigma(t, \gamma_0) = \gamma_0^2 G(t)$$

Constant shear rate  $\dot{\gamma}$ :

$$N_1(t, \dot{\gamma}) \approx 2\dot{\gamma}^2 \int_0^t du uG(u)$$

$$\sigma(t, \dot{\gamma}) \approx \dot{\gamma} \int_0^t du G(u)$$

Steady-state oscillation :

$$N_1(t) = S_{11}(t) - S_{22}(t) = \gamma_0^2 \{ G'(\omega) + [G''(\omega) - G''(2\omega)/2] \sin(2\omega t) \\ - [G'(\omega) - G'(2\omega)/2] \cos(2\omega t) \}$$

$$N_3(t) = S_{11}(t) - S_{33}(t) = (1 - \hat{\beta}) [S_{11}(t) - S_{22}(t)]$$

$$\hat{\beta} = -N_2/N_1, \text{ with } N_2 = N_3 - N_1$$

If  $G_n(t) = C G(t)$ :

Step strain of  $\gamma_0$ :

$$\Delta n \sin[2\chi_n((t, \gamma_0))] = 2C\sigma(t; \gamma_0) = 2C\gamma_0 G(t)$$

$$\Delta n \cos[2\chi_n((t, \gamma_0))] = CN_1(t; \gamma_0) = C\gamma_0^2 G(t)$$

$$\cot[2\chi_n((t, \gamma_0))] = N_1(t, \gamma_0)/2\sigma(t; \gamma_0) = \gamma_0/2$$

Constant shear rate  $\dot{\gamma}$ :

$$\Delta n \sin[2\chi_n(t, \dot{\gamma})] = 2C\sigma(t, \dot{\gamma}) = 2C\dot{\gamma} \int_0^t du G(u)$$

$$\Delta n \cos[2\chi_n(t, \dot{\gamma})] = CN_1(t, \dot{\gamma}) = C\dot{\gamma}^2 \int_0^t du uG(u)$$

$$\cot[2\chi_n(t, \dot{\gamma})] = N_1(t, \dot{\gamma})/2\sigma(t; \dot{\gamma}) = \dot{\gamma} \int_0^t du uG(u) / 2 \int_0^t du G(u)$$

elongation, respectively,[17g]

$$\mathbf{F}_{sh} = \begin{pmatrix} F_1[\gamma(t,u)] & 0 & 0 \\ 0 & F_1[\gamma(t,u)] & 0 \\ 0 & 0 & F_2[\gamma(t,u)] \end{pmatrix}$$

$$\mathbf{F}_{el} = \begin{pmatrix} F_3[\lambda(t,u)] & 0 & 0 \\ 0 & F_3[\lambda(t,u)] & 0 \\ 0 & 0 & F_3[\lambda(t,u)] \end{pmatrix}$$

$$\sigma(t) = \int_0^t du \frac{\partial G(u)}{\partial u} \gamma(t-u) F_1[\gamma(t-u)] \quad (88a)$$

$$N_1(t) = \int_0^t du \frac{\partial G(u)}{\partial u} \gamma(t-u)^2 F_1[\gamma(t-u)] \quad (88b)$$

$$\sigma(t, \dot{\gamma}) = - \int_0^t du \Delta\gamma(t,u) F_1[\Delta\gamma(t,u)] \frac{\partial G(u)}{\partial u} \quad (89)$$

$$N_1(t, \dot{\gamma}) = - \int_0^t du [\Delta\gamma(t,u)]^2 F_1[\Delta\gamma(t,u)] \frac{\partial G(u)}{\partial u} \quad (90)$$

$$\tau(t, \dot{\epsilon}) = - \int_0^t du \Delta\epsilon(t,u) F_3[\Delta\epsilon(t,u)] \frac{\partial E(u)}{\partial u} \quad (91)$$

for incompressible fluids, where  $\Delta\gamma(t,u) = (t-u)\dot{\gamma}$ , etc.

shear-rate dependent functions in steady-state flow given information on the linear viscoelastic shear relaxation modulus  $G(t)$ : [18; 43]

$$\begin{aligned}\eta(\dot{\gamma}) &= \eta H(\tilde{\beta}\tau_c\dot{\gamma}) \\ S^{(1)}(\dot{\gamma}) &= J_s S(\tilde{\beta}\tau_c\dot{\gamma}) \\ J_s(\dot{\gamma}) &= J_s P(\tilde{\beta}\tau_c\dot{\gamma})\end{aligned}$$

### 8. Strain-induced birefringence for concentrated and undiluted polymeric fluids.

Rheo-optical measurements have long been used in conjunction with rheological measurements. Examples include strain-induced birefringence, optical dichroism and light scattering. [16; 17h; 24c; 27; 97; 99; 115-120] Here only birefringence measurements will be discussed. The increasing availability of commercially available rheo-optical equipment afford enhanced opportunities for the use of birefringence techniques. For an isotropic material, the principal components (proper vectors)  $n_1$ ,  $n_2$  and  $n_3$  of the refractive index tensor are equal, but this symmetry is usually lost under deformation. Thus, in the shear and elongational deformations discussed above, with deformation in the 1,3-plane (in Cartesian coordinates), the birefringence  $\Delta n = n_1 - n_2$  measured by light propagating along  $x_3$  will generally not be zero, and the angle  $\chi_n \leq \pi/4$  between  $n_1$  and  $x_1$  will depend on the deformation. The angle  $\chi_n$  may be visualized by the orientation of the extinction cross of isocline viewed between crossed polars under appropriate optical arrangements. Several effects may contribute to the strain-induced optical anisotropy, including (i) orientation of optically anisotropic chain elements, and (ii) an internal field effect called "form birefringence" arising from spatial variations of the refractive index, as with the anisotropy in a deformed single chain in a dilute solution, or phase separated regimes in a blend, or a semicrystalline polymer. [17i; 27a] Here, consideration is limited to homogeneous amorphous polymers or their concentrated solutions, for which the form birefringence may be neglected. In the simplest case, of interest here, the optical anisotropy of the chain elements is assumed to have ellipsoidal symmetry, with a major axis along the chain axis, so that the optical anisotropy is directly associated with anisotropy of the chain conformation. [16e; 27b; 120] Clearly, that is a major approximation that may not always be valid, and deviations from the behavior anticipated with the simplification may provide insight on the material, [93; 121; 122] see examples cited below.

$$\Delta n = C\tau(\lambda) = (C/D_e)[D_e/D_e(\lambda)]\hat{\epsilon}_R(\lambda)$$

for a uniaxial elongation with stretch  $\lambda = 1 + \epsilon_{11}$  along  $x_1$  ( $\chi = 0$ ) under a tensile stress  $\tau = S_{11} - S_{22}$ , and

$$\begin{aligned}\Delta n \sin[2\chi_n(\dot{\gamma})] &= 2C\sigma(\dot{\gamma}) = 2(C/J_e)[J_e/J_e(\dot{\gamma})]\hat{\gamma}_R(\dot{\gamma}) \\ \Delta n \cos[2\chi_n(\dot{\gamma})] &= CN_1(\dot{\gamma}) \\ \cot[2\chi_n(\dot{\gamma})] &= N_1(\dot{\gamma})/2\sigma(\dot{\gamma}) = m\hat{\gamma}_R(\dot{\gamma})\end{aligned}$$

Steady-state response to a small amplitude oscillatory shear deformation:[99; 125]

$\omega$ . [99]

Transient strain-induced birefringence

Approximation  $G_n(t)/G(t) = C$ :

for a sample relaxed for  $t < 0$ . Thus, for an elongational deformation ( $\chi_n = 0$ ) of an incompressible viscoelastic solid under a strain-defined history resulting in a transient stress  $\tau(t) = S_{11}(t) - S_{22}(t)$  and transient strain  $\epsilon(t) = \epsilon_{11}(t)$  for deformation along  $x_1$ ,

$$\Delta n(t) = C\tau(t) = 3C \int_0^t du G(t-u) \frac{\partial \epsilon(u)}{\partial u}$$

Similarly, for a recently small shear deformation to obtain a linear viscoelastic response,  $\Delta n(t) = 2n_{12}(t)\sin[\chi_n(t)]$ , so that since in this case  $\sin[2\chi_n(t)] \approx 1$ , the preceding gives

Steady-state shear flow in the linear response:

$$\Delta n = 2C\dot{\gamma} \int_0^\infty du G(u) = 2C\eta\dot{\gamma} = 2(C/J_s)\hat{\gamma}_R(\dot{\gamma})$$

with  $\hat{\gamma}_R(\dot{\gamma})$  the total strain recoil on cessation of flow.

An important use of strain-induced birefringence measurements is in the estimation of the first-normal stress difference  $N_1(t)$  in a transient response in a strongly nonlinear response. Neither  $N_1(t; \gamma_0)$  in relaxation following a step-strain  $\gamma_0$  nor  $N_1(t; \dot{\gamma})$  in shear deformation in nonlinear flows at a constant shear rate are trivial to measure mechanically. For example, although  $N_1(t; \dot{\gamma})$  may be determined from the force required to prevent separation of a cone and plate during a shear deformation, the slight movement unavoidable in the feedback mechanism to produce a measure of the required force may complicate the interpretation of the transient response.[128] The error should be less serious in a steady flow.

## Steady-state flow

Step-strain  $\gamma_0$  in the 1,2-plane gives

$$\begin{aligned}\Delta n \sin[2\chi_n(t; \gamma_0)] &= 2C\sigma(t; \gamma_0) = 2C\gamma_0 F(\gamma_0)G(t) \\ \Delta n \cos[2\chi_n(t; \gamma_0)] &= CN_1(t; \gamma_0) = C\gamma_0^2 F(\gamma_0)G(t) \\ \cot[2\chi_n(t; \gamma_0)] &= N_1(t; \gamma_0)/2\sigma(t; \gamma_0) = \gamma_0/2\end{aligned}$$

.[129; 130]

Steady-state shear flow,

$$\begin{aligned}\Delta n \sin[2\chi_n(t; \dot{\gamma})] &= 2C\sigma(t; \dot{\gamma}) \\ \Delta n \cos[2\chi_n(t; \dot{\gamma})] &= CN_1(t; \dot{\gamma}) \\ \cot[2\chi_n(t; \dot{\gamma})] &= N_1(t; \dot{\gamma})/2\sigma(t; \dot{\gamma}) = S^{(1)}(t; \dot{\gamma})\sigma(t; \dot{\gamma})\end{aligned}$$

for the 1,2-plane, with  $\sigma(t; \dot{\gamma})$  and  $N_1(t; \dot{\gamma})$  computed as discussed in the section on nonlinear viscoelasticity,  $\chi_n(t; \dot{\gamma}) \leq \pi/4$  decreases with increasing  $\dot{\gamma}$ , and. Similarly,  $\Delta n_{1,3}(t; \dot{\gamma}) = C(1 - \hat{\psi})N_1(t; \dot{\gamma})$  in the 1,3-flow plane in this approximation if it is assumed that  $\hat{\psi}$  is independent of  $t$  and  $\dot{\gamma}$ . At steady-state flow, these relations become

$$\Delta n \sin[2\chi_n(\dot{\gamma})] = 2C\sigma(\dot{\gamma}) = 2(C/J_s)[J_s/J_s(\dot{\gamma})]\hat{\gamma}_R(\dot{\gamma})$$

$$\Delta n \cos[2\chi_n(\dot{\gamma})] = CN_1(\dot{\gamma}) = 2(C/J_s)[S^{(1)}(\dot{\gamma})/J_s(\dot{\gamma})][J_s/J_s(\dot{\gamma})]\hat{\gamma}_R(\dot{\gamma})^2$$

$$\cot[2\chi_n(\dot{\gamma})] = N_1(t; \dot{\gamma})/2\sigma(t; \dot{\gamma}) = S^{(1)}(\dot{\gamma})\sigma(\dot{\gamma}) = [S^{(1)}(\dot{\gamma})/J_s(\dot{\gamma})]\hat{\gamma}_R(\dot{\gamma})$$

where

$$S^{(1)}(t; \dot{\gamma}) = N_1(t; \dot{\gamma})/2[\sigma(t; \dot{\gamma})]^2$$

$$\sigma(\dot{\gamma}) = \dot{\gamma}\eta(\dot{\gamma})$$

$\hat{\gamma}_R(\dot{\gamma}) = J_s(\dot{\gamma})\dot{\gamma}\eta(\dot{\gamma})$  is the total recoverable strain following cessation of steady-state flow. Similarly,  $\Delta n_{1,3}(\dot{\gamma}) = C(1 - \hat{\psi})N_1(\dot{\gamma})$  in the 1,3-flow plane if it is assumed that  $\hat{\psi}$  is independent of  $\dot{\gamma}$ . The final forms emphasize the relation of the birefringence to the constrained recoil  $\hat{\gamma}_R(\dot{\gamma})$  on cessation of flow, and are analogous to the relations given above for an elastic solid (i.e., replace  $\dot{\gamma}$  by  $\gamma$ ,  $J_s$  by  $J_e$  and  $S^{(1)}(\dot{\gamma})/J_s(\dot{\gamma})$  by  $m$ ). As discussed in the previous section,  $S^{(1)}(\dot{\gamma})/J_s(\dot{\gamma})$  depends on the distribution of components (e.g., the molecular weight distribution), where  $S^{(1)}(\dot{\gamma})/J_s(\dot{\gamma}) \leq 1$ , with the equality occurring for flows of monodisperse polymer with  $\tau_c\dot{\gamma} < 1$ . The analogy with the behavior for a linear elastic solid is strengthened by noting that  $S^{(1)}(\dot{\gamma})/J_s(\dot{\gamma})$  tends toward 0.5 with increasing  $\tau_c\dot{\gamma}$ , similar to the value of  $m$  noted above for a linear elastic solid, as remarked above. Estimates of  $N_1(t; \dot{\gamma})$  made in this way appear to be similar to those obtained by direct mechanical measurements.[106; 107; 109; 110] This correspondence could reflect the marked weighting of the response toward the longer time response in  $G_n(t)$ , and may not provide definitive evidence for constant  $G_n(t)/G(t)$  for all  $t$ . In part, the use of the stress-optic approximation here is motivated by statistical mechanical theories which suggest that  $\Delta n$  and  $\Delta S$  depend on similar averages over chain conformations for flexible chain polymers,[16h; 22h; 27b; 120] but the similarity with the expression for an elastic solid given above is evident, and is not accidental since the theories in both cases are based on additivity of incremental stresses attributed to molecular deformations, similar to the treatment of a collection of macroscopic beads and dashpots.[22h]

Relations comparable to the preceding do not appear to be available for a stress-defined history. Moreover, there are few data to evaluate the nature of  $J_n(t)$ , a situation that may change with the availability of commercial rheo-optical instrumentation to permit the implementation of stress-defined histories. The lack of experimental and theoretical attention may reflect both the lack of commercially available equipment to study the transient response with a stress-defined shear deformation and the perception that  $J_n(t)$  is a constant, as required by the stress optic approximation with constant  $G_n(t)/G(t)$ , in which case birefringence measurements for a stress-defined history would be relatively uninteresting. However, as remarked in the preceding, the evidence that  $G_n(t)/G(t)$  must be considered to be independent of  $t$  is not definitive. For example,  $G_n(t)$  could relax more slowly than  $G(t)$  for large  $t$ , but still decay fast enough to give the response  $G'_n(\omega) \propto \omega^2$  and  $G''_n(\omega) \propto \omega$  reported experimentally for small  $\omega$ . [100] In addition, as may be seen in the

expression for  $J_n(t)$ , deviation of  $G_n(t)/G(t)$  from a constant for small  $t$  will have an impact on  $J_n(t)$  at large  $t$ . As mentioned above, birefringence measurements are sometimes made on amorphous materials near  $T_g$ , with the finding that a single constant  $C$  cannot be applied over the entire range of  $\omega$  at a given  $T$ . [126; 127] This result is readily accommodated in terms of a distribution of retardation times to represent  $\alpha(t)$ , with the response corresponding to an Andrade creep region having a different value of  $C$  than that associated with the portion of the retardation times associated with the Rouse-like or entanglement responses.

Given the uncertain status of the stress-optic approximation, it is of interest to consider the consequences of a strain-optic approximation for use with stress-defined experiments. Since the birefringence is a constant in steady-state flow, it is apparent that  $J_n(t)$  must not have the term proportional to  $t$  found in  $J(t)$ , even if  $J_n(t)$  is not a constant as required by the stress-optic approximation. Further, the preceding provides a clear relationship between the birefringence and the recoverable strain for an elastic solid under a small deformation and a fluid in a slow steady-state flow. For lack of a definitive treatment, it will be assumed that these features are preserved in a transient deformation, and that the birefringence at arbitrary time is related to the total constrained recoil that would be recovered if the stress were suddenly reduced to zero at that time; the calculation of this following an arbitrary stress history is discussed above in the section on creep and recovery in the section on linear viscoelastic phenomenology. Thus, for recently small deformations on an incompressible sample relaxed at the beginning of the deformation, such that the linear viscoelastic response functions may be used, it is presumed that  $J_n(t) = (C/J_\infty)R(t)$ , and that the deviatoric components of the refraction tensor are given by,

$$n_{ij}(t) = (C/J_\infty) \int_0^t ds R(t-s) \left[ \frac{\partial S_{ij}(s)}{\partial s} - \frac{1}{3} \delta_{ij} \frac{\partial S_{\alpha\alpha}(s)}{\partial s} \right]$$

Consequently, for elongational or shear deformations, with total recoverable strains  $\hat{\epsilon}_R(t)$  and  $\hat{\gamma}_R(t)$ , respectively,

$$\Delta n(t) = (C/D_\infty) \hat{\epsilon}_R(t) = (C/3D_\infty) \int_0^t du R(t-u) \frac{\partial \tau(u)}{\partial u} \quad (124a)$$

$$\Delta n(t) = 2(C/J_\infty) \hat{\gamma}_R(t) = 2(C/J_\infty) \int_0^t du R(t-u) \frac{\partial \sigma(u)}{\partial u} \quad (124b)$$

For example, for a step stress  $\sigma_0$  initiated at zero time, and terminated at time  $T_e$  on a linear viscoelastic fluid

$$\Delta n(t) = 2(C/J_s)\sigma_o \int_0^t du R(t-u) \delta(u-0) = 2(C/J_s)R(t)\sigma_o \quad (125)$$

At a time  $\vartheta$  following the onset of constrained recoil after creep terminated at time  $t = T_e$ ,

$$\Delta n(\vartheta) = 2(C/J_s)\{\hat{\gamma}_R(T_e) - \hat{\gamma}_R(\vartheta)\} \quad (126a)$$

$$= 2(C/J_s)\{R(\vartheta + T_e) - R(\vartheta)\}\sigma_o \quad (126b)$$

Strict application of the stress-optic approximation would make  $\Delta n$  independent of time by contrast with these expressions, but data to evaluate these alternatives do not seem to be available. In an alternative deformation history, the total recoverable strain  $\hat{\gamma}_R(T_e, \gamma_o)$  that would be measured if the stress were dropped to zero at time  $T_e$  during stress relaxation of a fluid following a jump  $\gamma_o$  in the strain is given above by  $\hat{\gamma}_R(T_e, \gamma_o) = \gamma_o[1 - \eta^{-1} \int_0^{T_e} ds G(s)]$ . With this expression,  $\Delta n(t) \approx 2(C/J_s)\hat{\gamma}_R(t, \gamma_o)$  is not equal to the relation  $\Delta n(t) \approx 2CG(t)$  given above using the stress-optic approximation, unless  $G(t)$  is given by an exponential function, in which case  $R(t)$  is a constant, as would be consistent with the stress-optic approximation.

A few studies are available for a step stress  $\tau_o$  initiated at zero time, and terminated at time  $T_e$  on a linear viscoelastic solid, for which  $D(t) \approx R(t)/3$ ,

$$\Delta n(t) = (C/D_e)\tau_o D(t) \quad 0 < t < T_e \quad (127a)$$

$$\Delta n(\vartheta) = (C/D_e)\tau_o [D(\vartheta + T_e) - D(\vartheta)] \quad t \geq T_e \quad (127b)$$

where  $\vartheta = t - T_e$ . Thus, if  $T_e$  is large enough that  $D(t)$  approaches its equilibrium value  $D_e$  during creep, then  $\Delta n(\vartheta)/C\tau_o = D_e - D(\vartheta)$  during recovery ( $t \geq T_e$ ). A recent study on a loosely crosslinked rubber may illustrate the delicacy of birefringence measurements.[131] Whereas the data on the strain in creep and recovery appear qualitatively normal, the birefringence was observed to be positive in creep, and negative in recovery. The numerous dangling chains (chains attached only once to the network) may provide an explanation for this unexpected behavior if these chains relaxed during creep, and were subsequently oriented orthogonal to the stretch direction during the relatively large initial recovery, so that  $\Delta n$  was subsequently negative during recovery for  $t > T_e$ . This would provide an example of the failure of the initial assumption concerning the origin of the birefringence introduced above.

Application to nonlinear deformations is less readily evaluated. Steady-state shear flow reached by a stress or strain defined histories must be equivalent. As seen in the preceding, in such a case  $\cot[2\chi_n(\dot{\gamma})] = [S^{(1)}(\dot{\gamma})/J_s(\dot{\gamma})]\hat{\gamma}_R(\dot{\gamma})$ , with  $S^{(1)}(\dot{\gamma})/J_s(\dot{\gamma}) \approx 1$  if the flow deformation may be characterized by use of  $\mathbf{Q}_0$ . The function  $\cot[2\chi_n(t; \sigma_0)]$  in linear or nonlinear creep under a step-stress  $\sigma_0$  must approach this behavior in steady-state flow. Thus, using the constrained recoil  $\hat{\gamma}_R(t; \sigma_0)$  on removal of the stress at time  $t$ , one might expect that

$$\cot[2\chi_n(t; \sigma_0)] = \Phi(t; \sigma_0)\hat{\gamma}_R(t; \sigma_0) \quad (129)$$

where  $\eta(t; \dot{\gamma}) = \sigma(t; \dot{\gamma})/\dot{\gamma}$ ,  $R(t; \sigma_0) = \hat{\gamma}_R(t; \sigma_0)/\sigma_0$ , and  $\Phi(t; \sigma_0) = S^{(1)}(t; \sigma_0)/R(t; \sigma_0)$ . Presumably,  $\Phi(t; \sigma_0)$  will vary from about unity for small  $t$ , since then the strain must be recently small, to its limiting value of about 0.5 in steady-state nonlinear flow. In principle,  $\Phi(t; \sigma_0)$  could be estimated by an interative calculation involving the relations given in the section on nonlinear rheological behavior, as has been done for  $J_s(\dot{\gamma})$ . [43]

In summary, it appears that the stress-optic approximation, embodied in the expression  $G_n(t)/G(t) \approx C$  for all  $t$ , may sometimes be used for strain-defined deformations to estimate the first-normal stress and the shear stress in a shear deformation, and the tensile stress in an elongational deformation, although it is clear that the approximation is not always valid, especially for deformation involving the short-time features of the response, e.g., the transition from the Andrade creep to the Rouse-like response in the retardation spectrum. The experimental situation is not clear for stress-defined deformations, with strict compliance with the relation  $G_n(t)/G(t) \approx C$  requiring that  $J_n(t)$  be independent of time. An alternative approximation may be to put  $J_n(t)/R(t) \approx C/J_\infty$  in a strain-optic approximation, with neither the stress-optic or strain-optic relations expected to be exact.

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